



Optimization of Crossing Geometry in Railway Turnouts

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SIMPACK User Meeting

Salzburg

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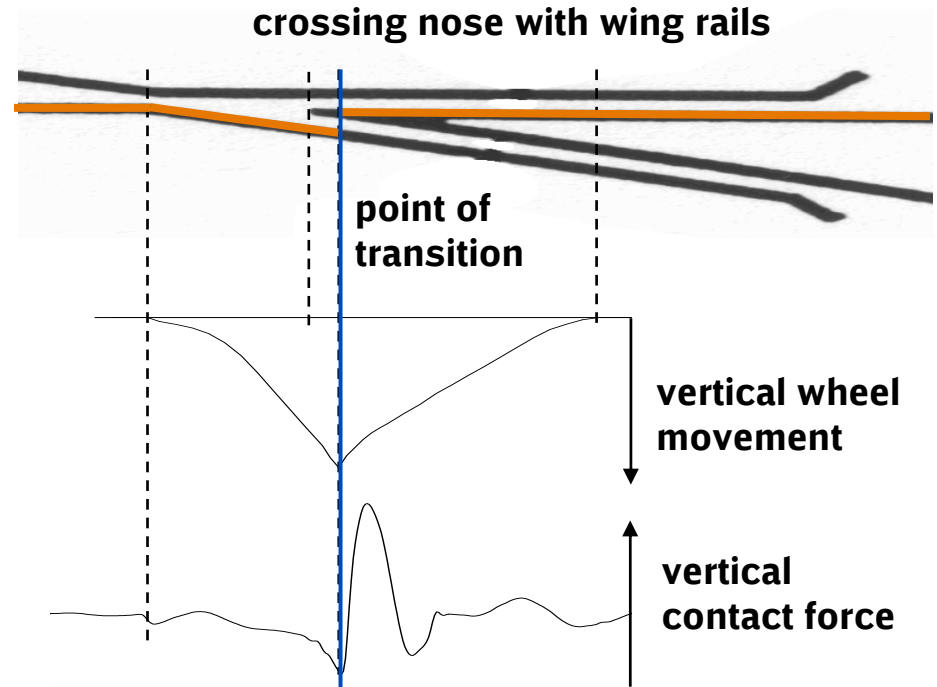
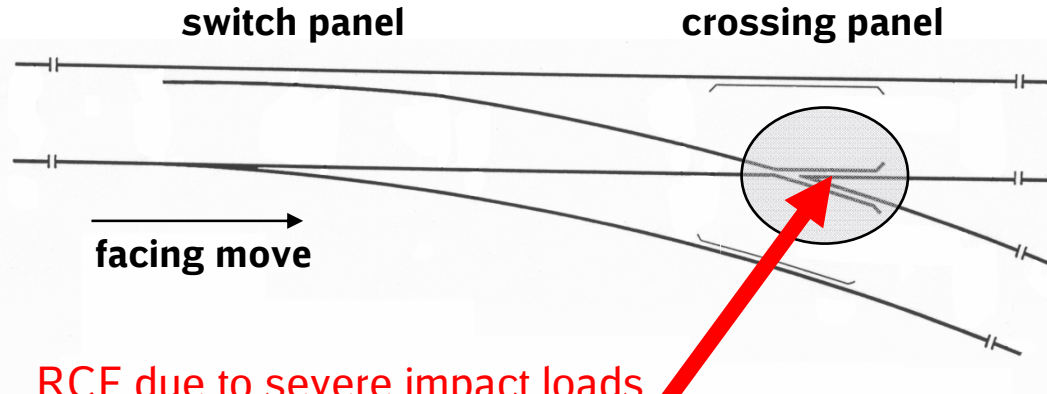


Overview

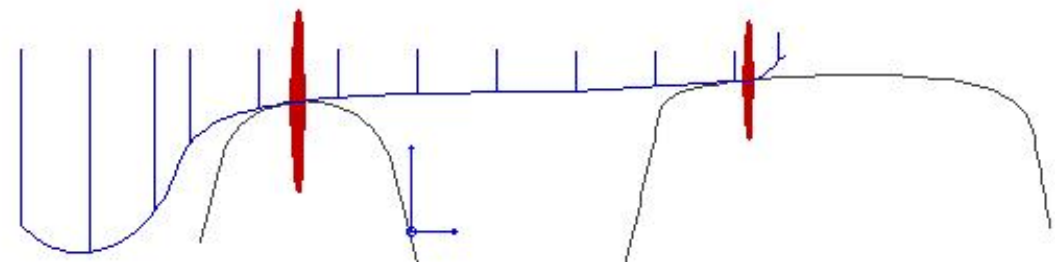
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- 2. Simulation model and model validation**
- 3. Investigation of alternative crossing designs**
- 4. Simulation of material degradation in service**
- 5. Conclusion and future work**

Introduction



Damage on running surface of crossing nose





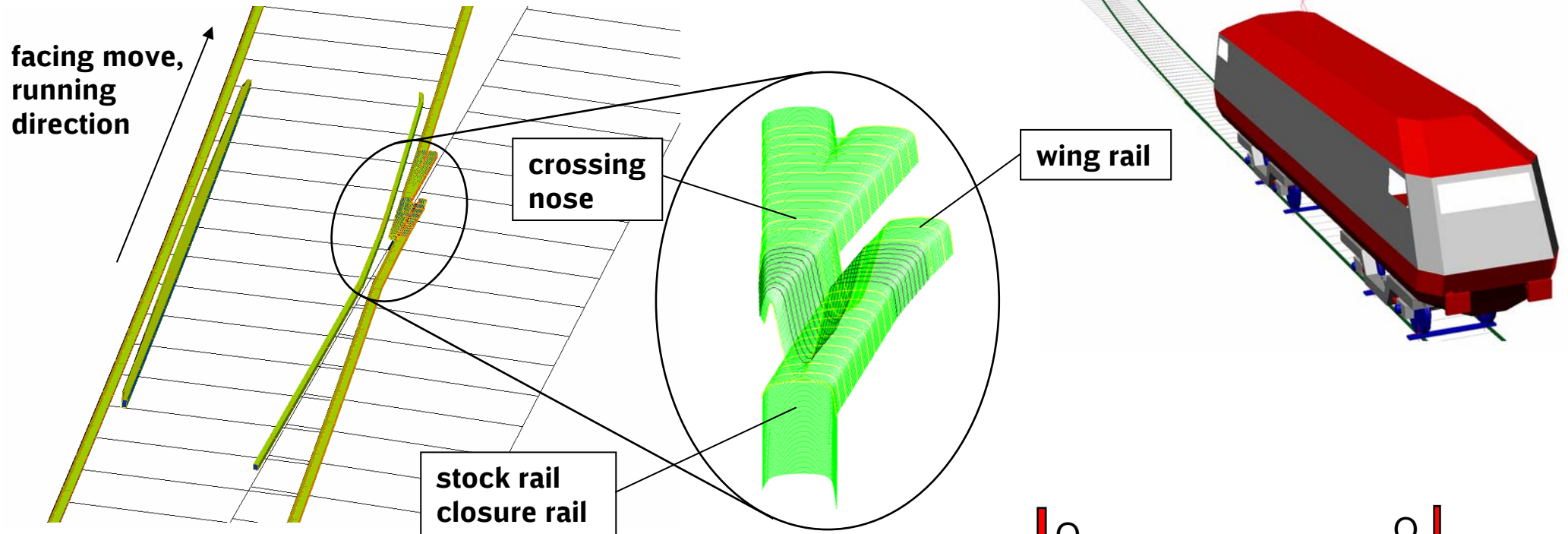
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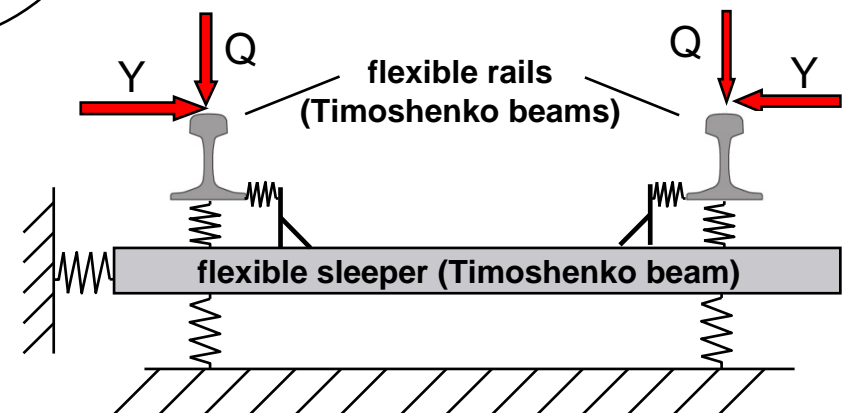
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SIMPACK simulation model

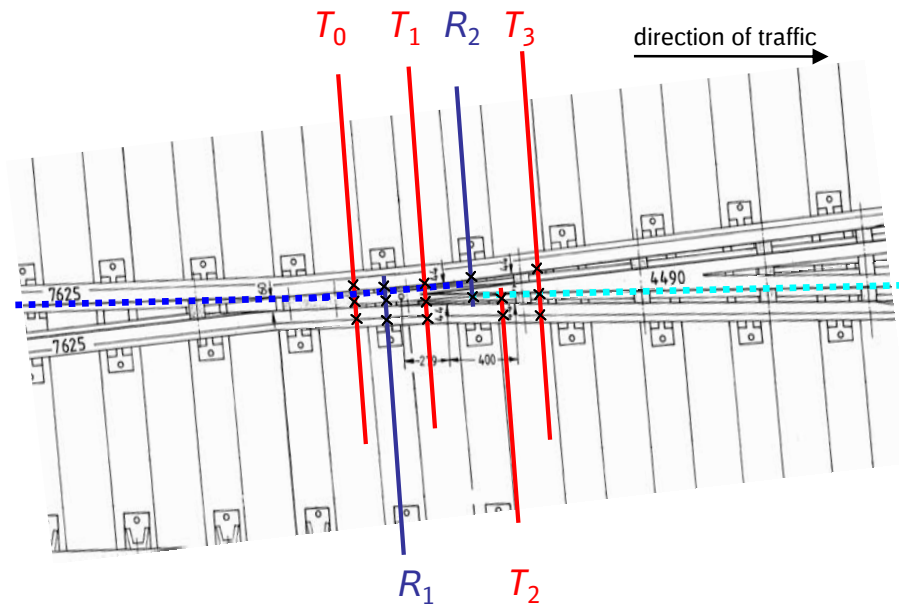


Elastic track model (FEM) implemented in SIMPACK (user routine of DB Netz AG)



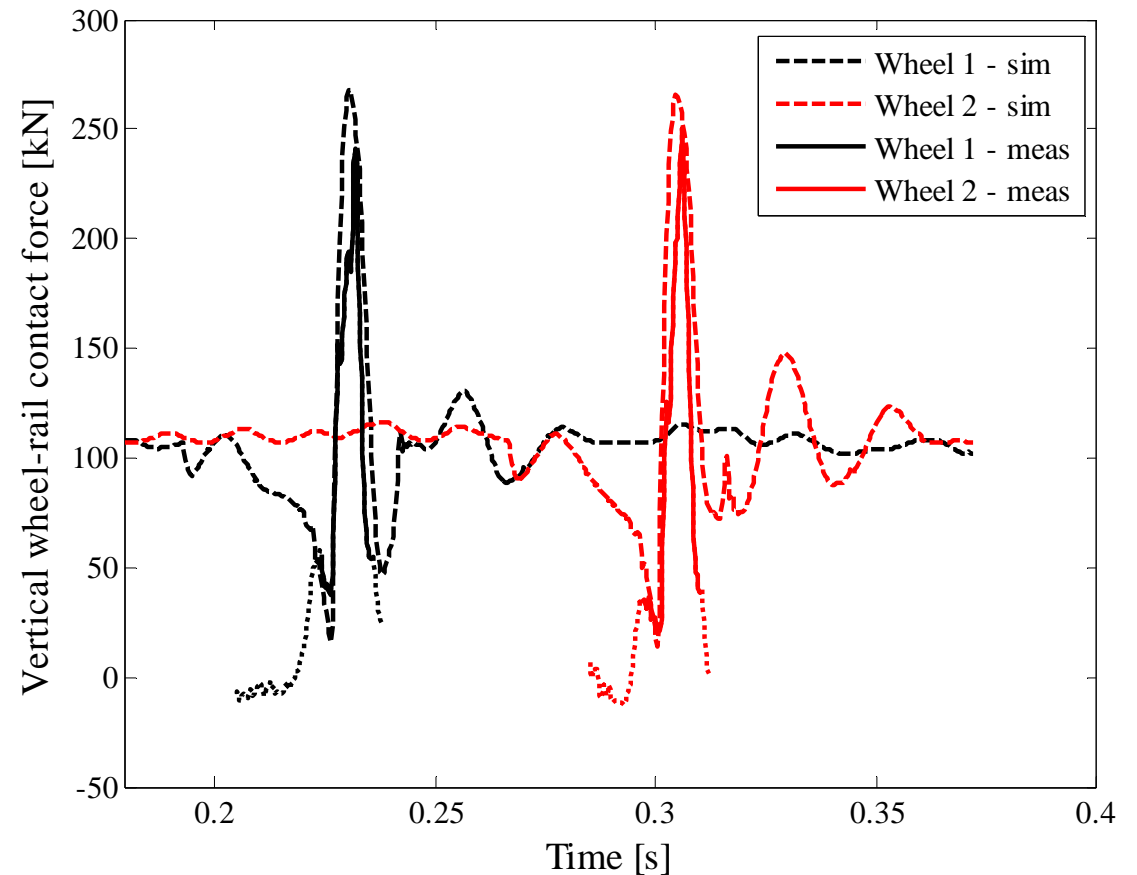
Model validation

Comparison of measured and simulated vertical contact forces of two passing wheels



Positions of strain gauges (x)
(T_i – shear forces, R_j – rail seat forces)

$$\text{Summation: } Q = T_0 + R_1 + R_2 + T_3$$





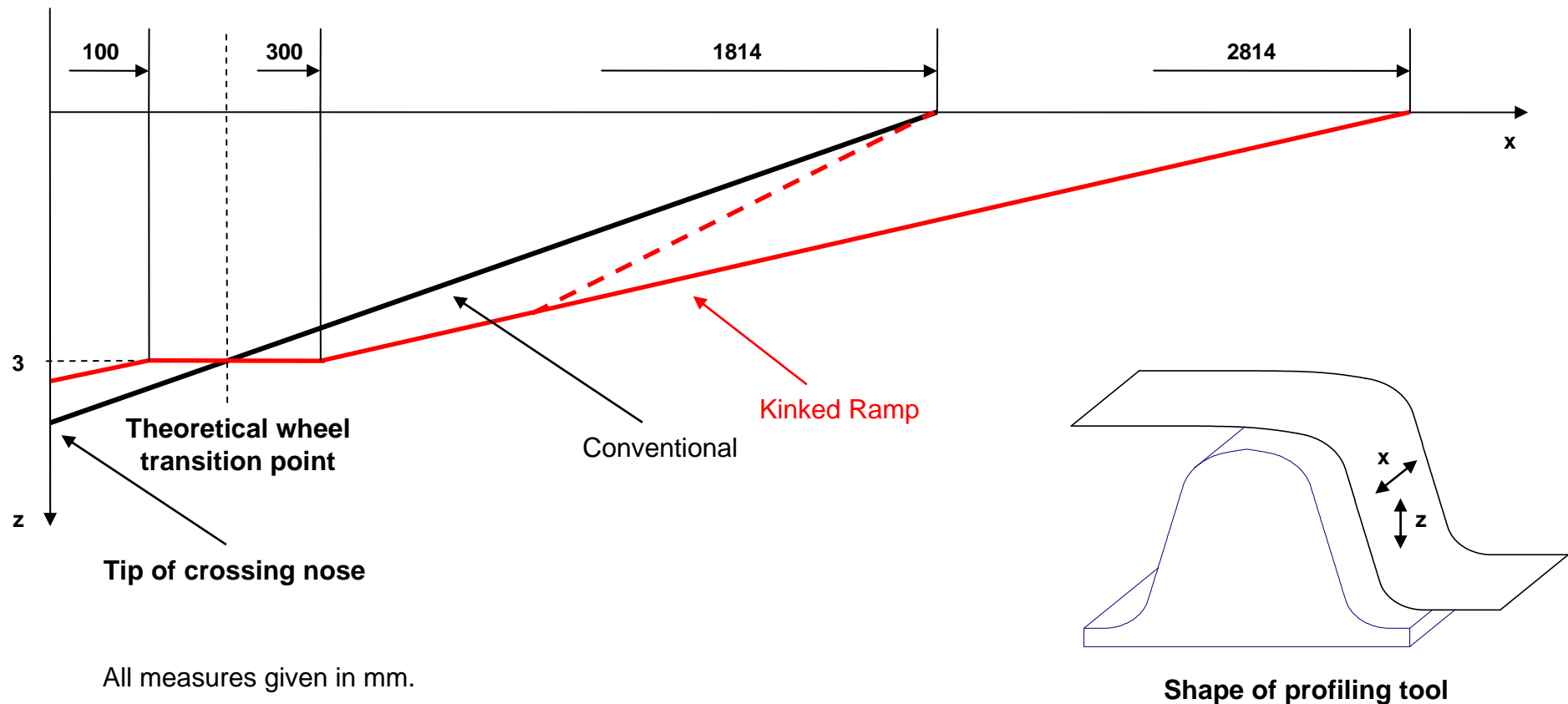
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Optimization of geometry

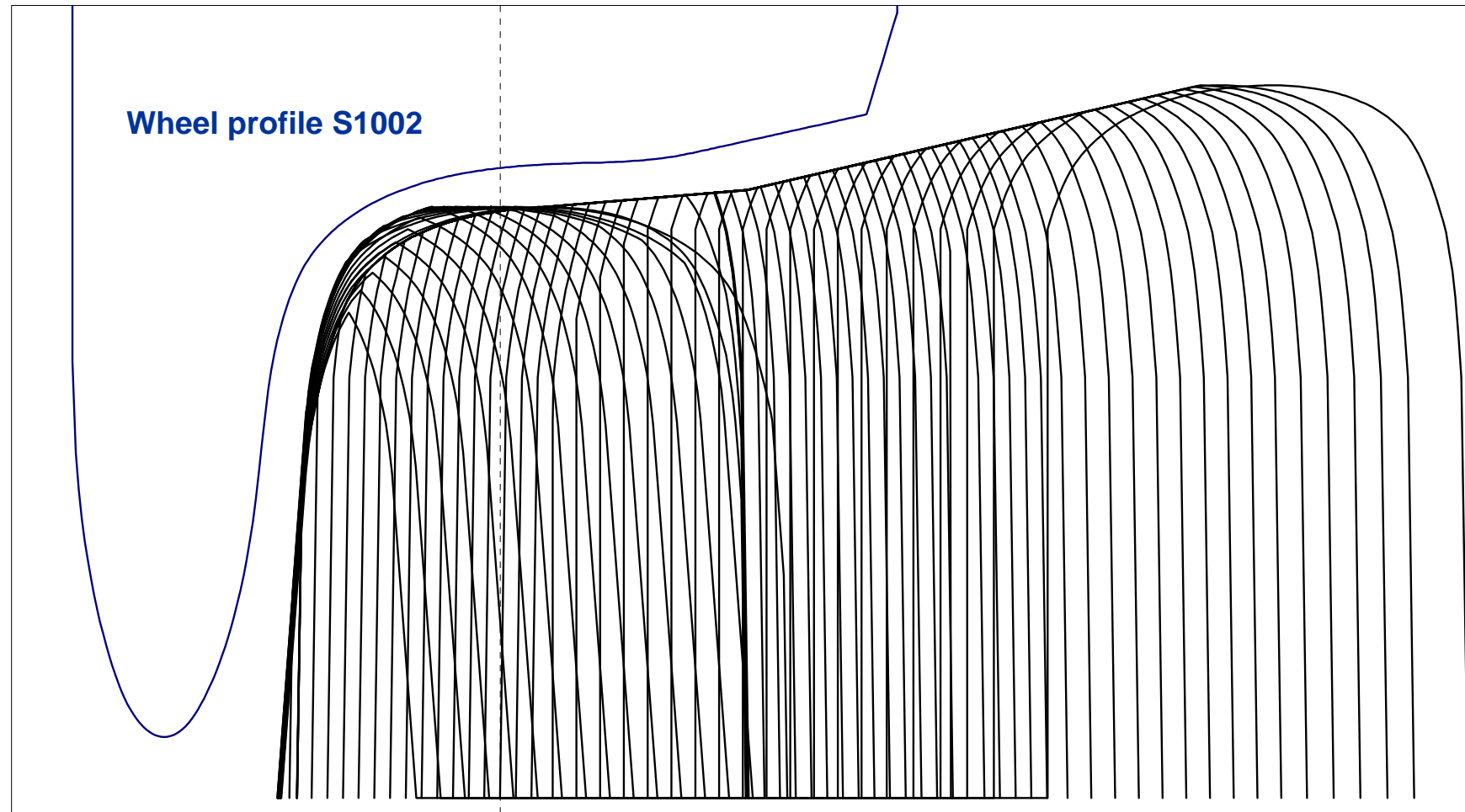
Crossing geometry „Kinked Ramp“ for EH 60-500-1:12 (Trajectory of profiling tool)





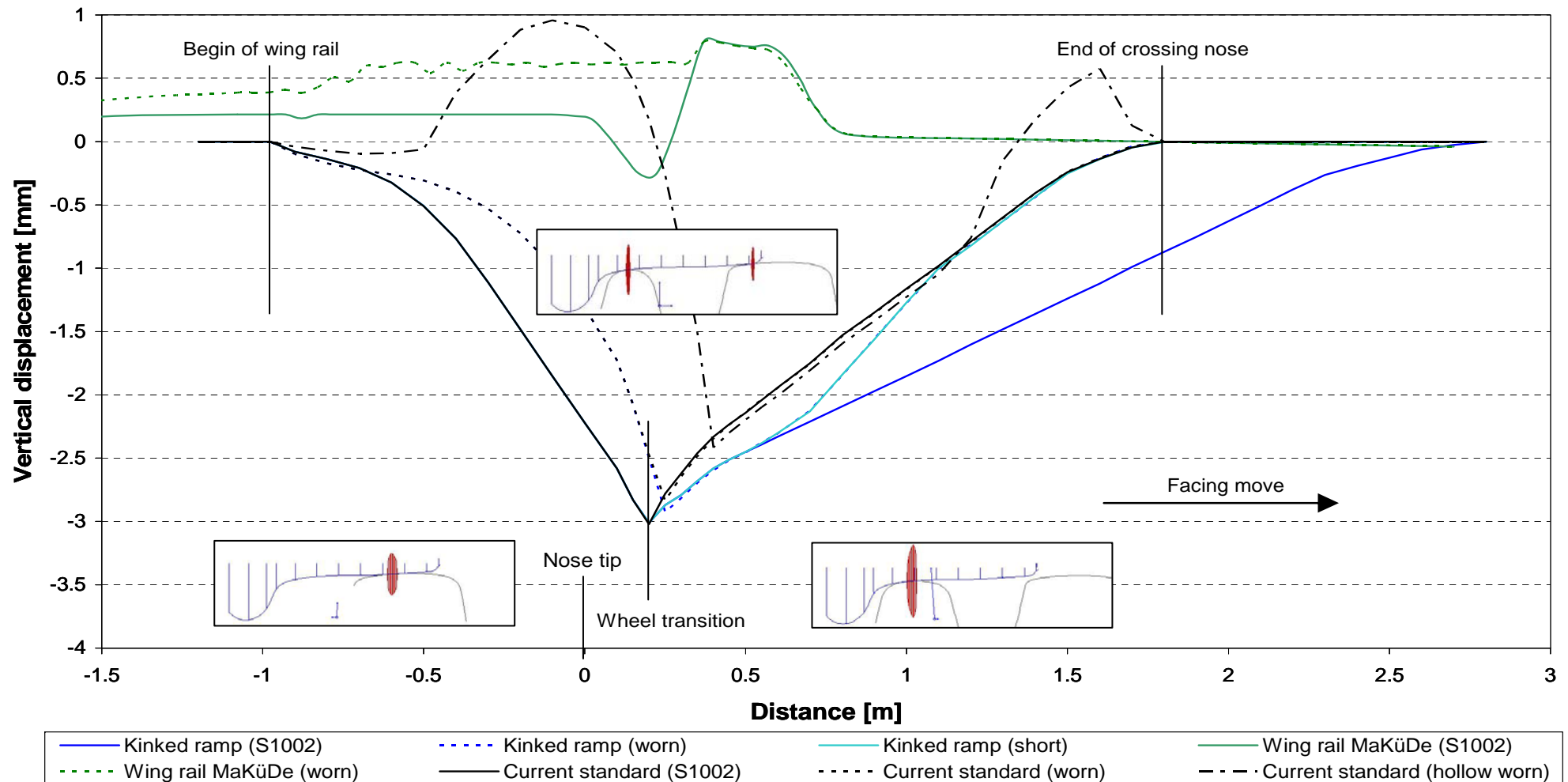
Optimization of geometry

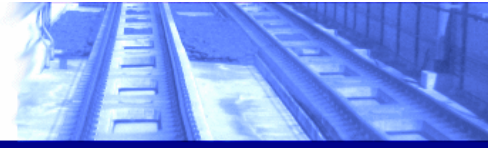
Crossing geometry „MaKüDe“ for EH 60-500-1:12



Vertical wheel movement

Comparison of vertical wheel movement (quasi-static)





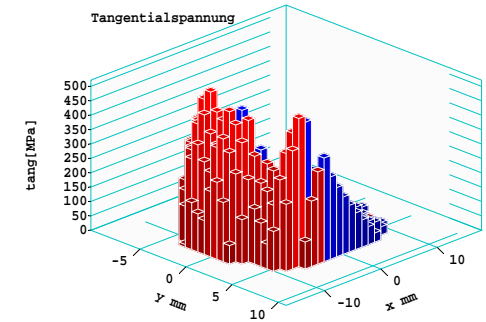
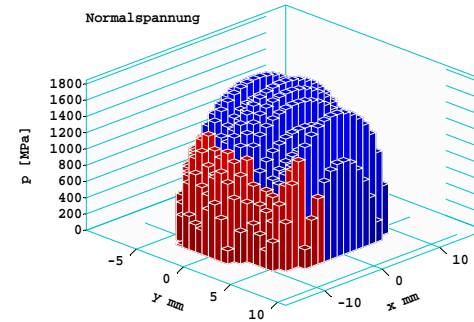
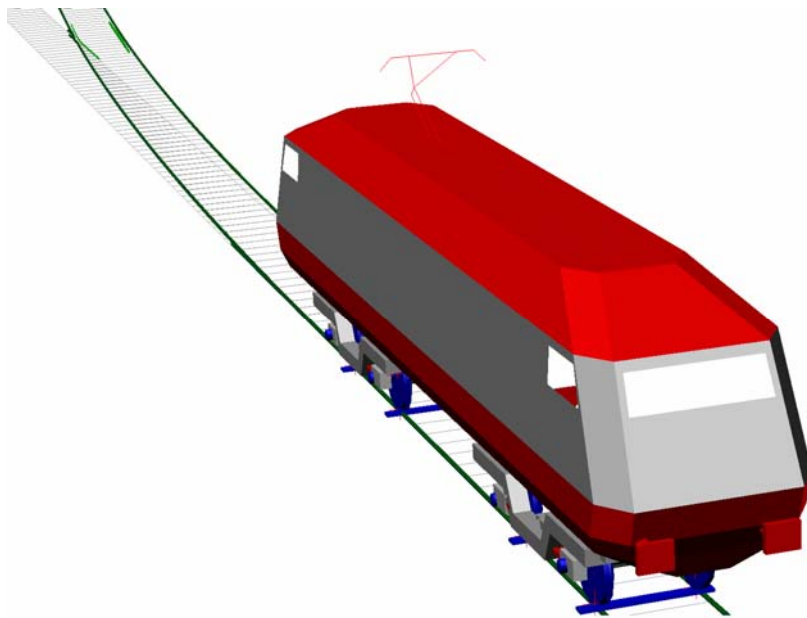
Evaluation of Contact Stresses

MBS simulation



Creepages, Friction coeff.,
Penetration in contact patch

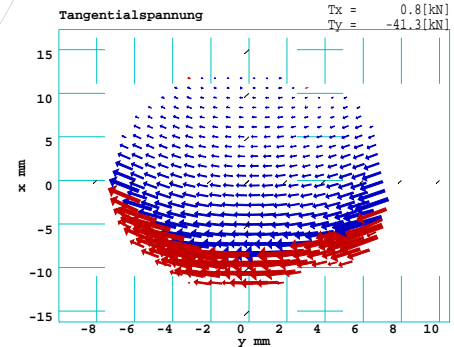
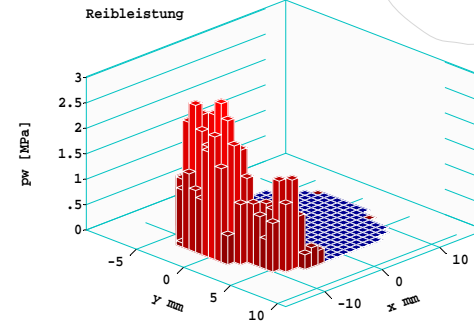
3D Stress calculation



$p_{max}(16,16) i(0.5, 0.3)mm = 1848. [MPa]$
 $sv_{max}(10,24) i(-6.2, 5.7)mm = 1096. [MPa]$
 $sl_{max}(16,16) i(0.5, 0.3)mm = 2793. [MPa]$
 $ta_{max}(10,24) i(-6.2, 5.7)mm = 1252. [MPa]$

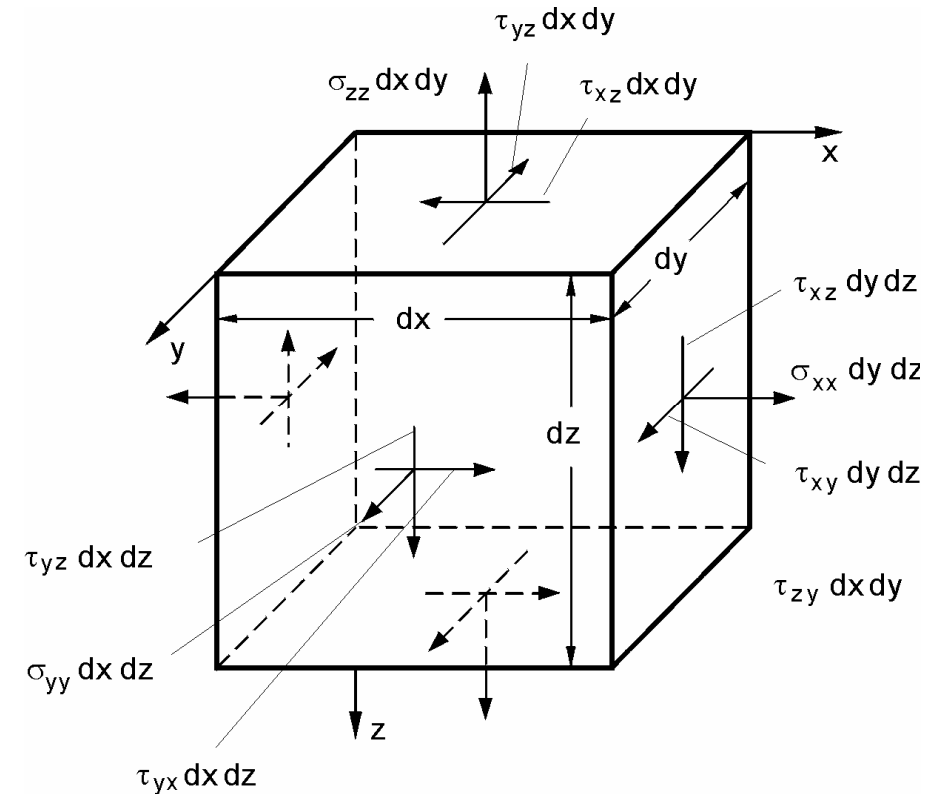
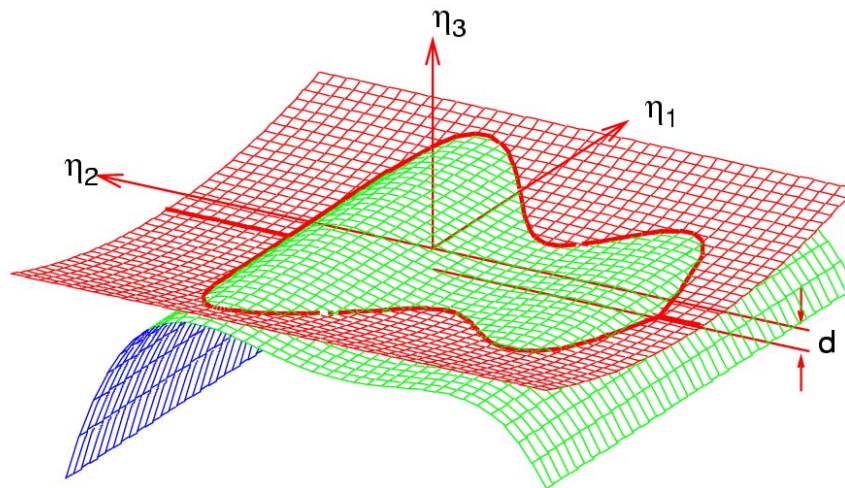
Durchdringung

$N = 333.3 [kN]$
 $TT = 41.3 [kN]$
 $TX = 0.8 [kN]$
 $TY = -41.3 [kN]$



Equivalent Contact Stress

Calculation of equivalent contact stresses according to v. Mises

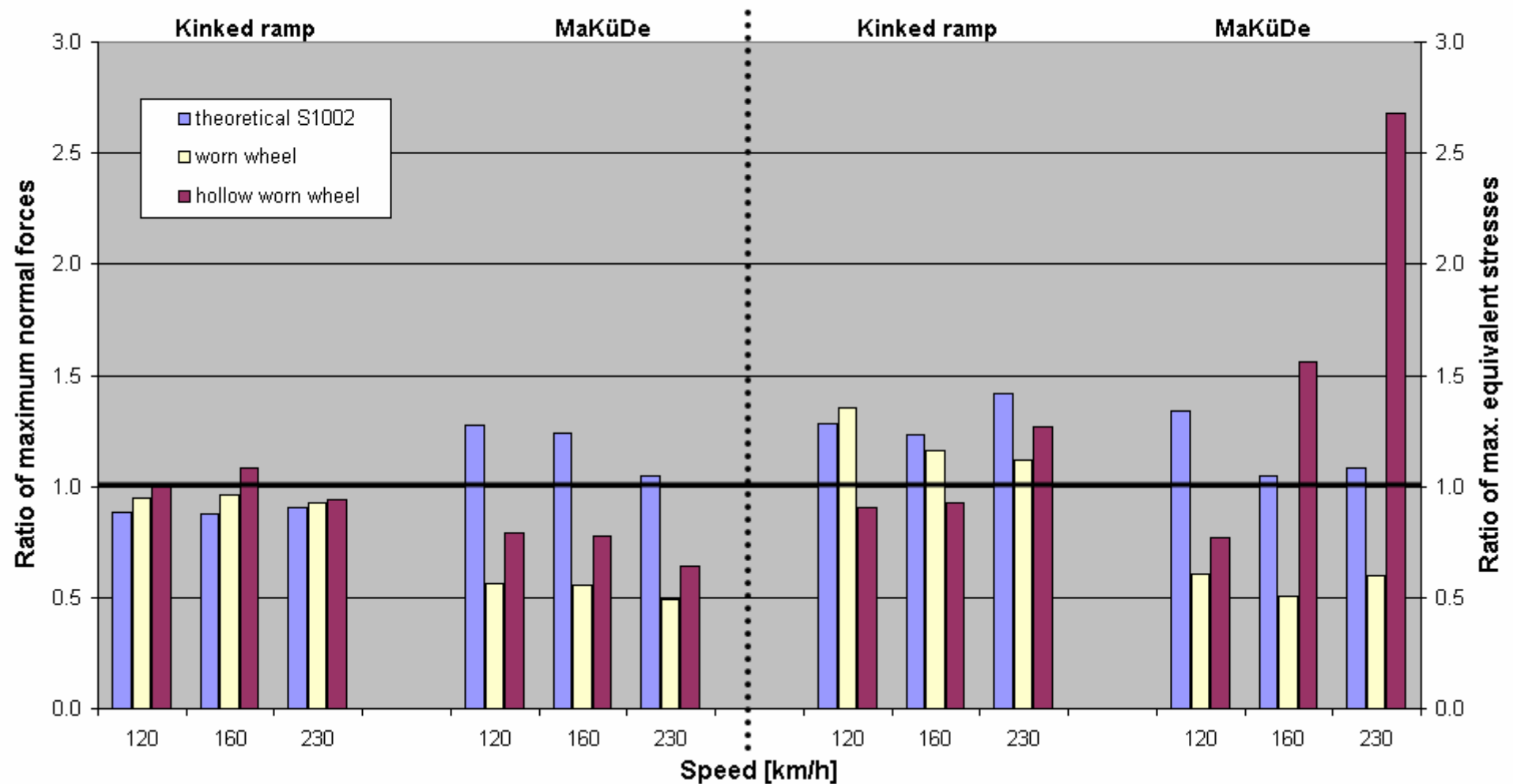


$$\sigma_e = \sqrt{\frac{1}{2} [(\sigma_{xx} - \sigma_{yy})^2 + (\sigma_{yy} - \sigma_{zz})^2 + (\sigma_{zz} - \sigma_{xx})^2] + 3 \cdot (\tau_{xy}^2 + \tau_{yz}^2 + \tau_{zx}^2)}$$



Discussion of simulation results

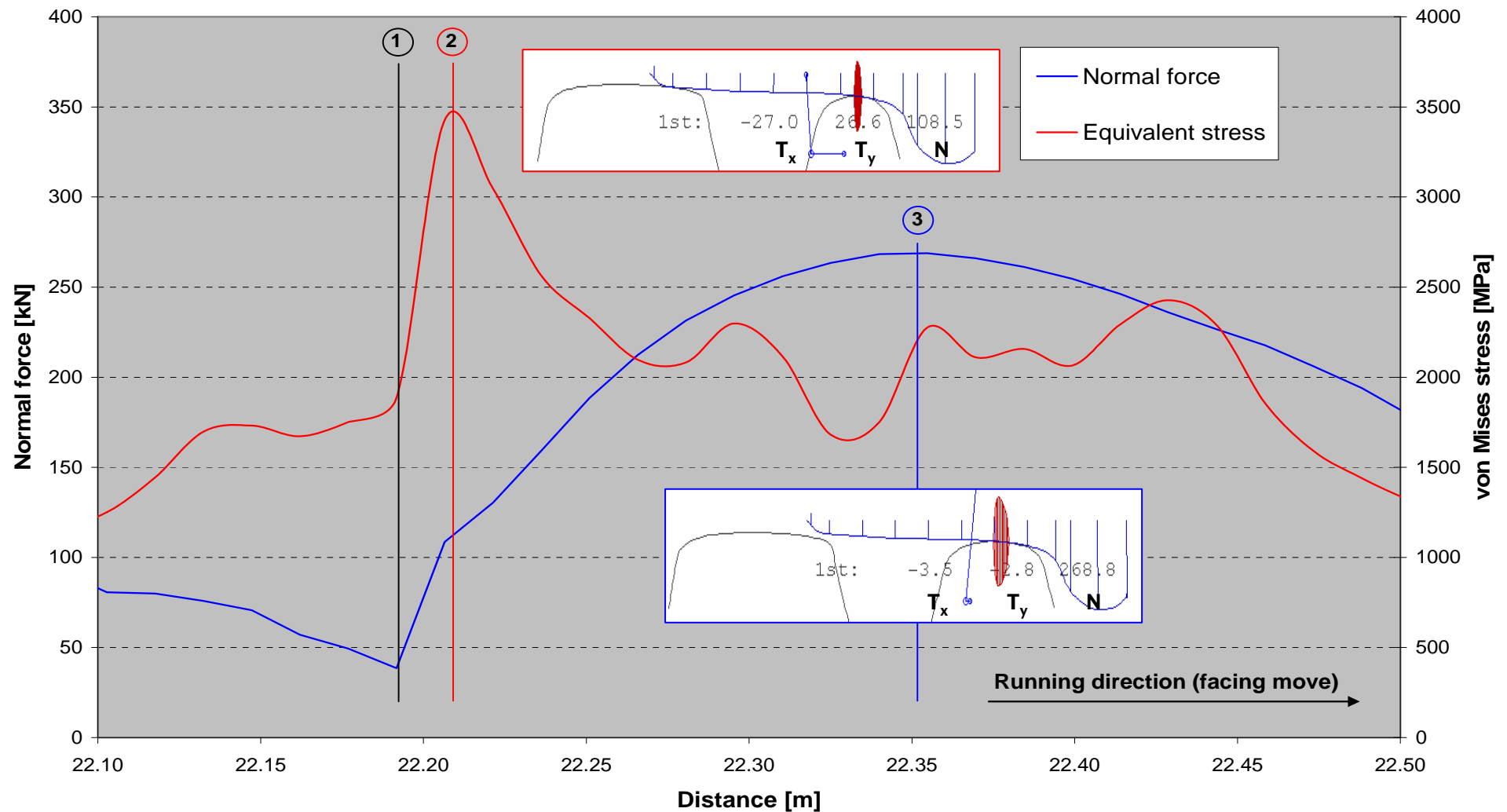
Normal forces and equivalent stresses in relation to Standard geometry





Discussion of simulation results

Time histories of Normal force and von Mises stress



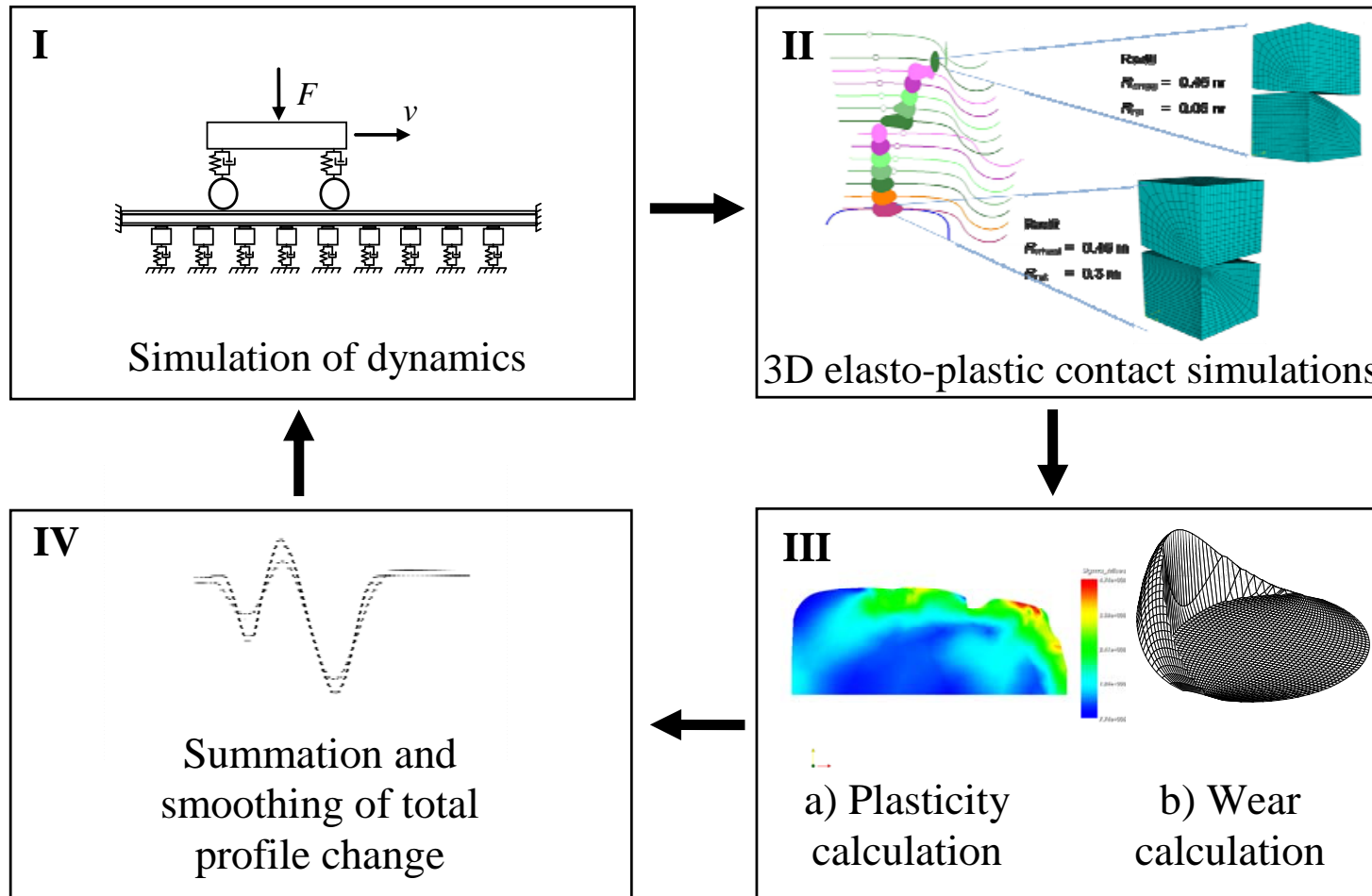


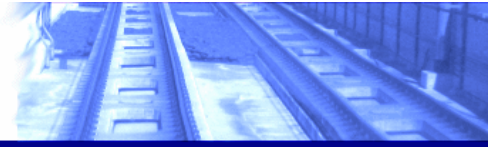
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Simulation methodology

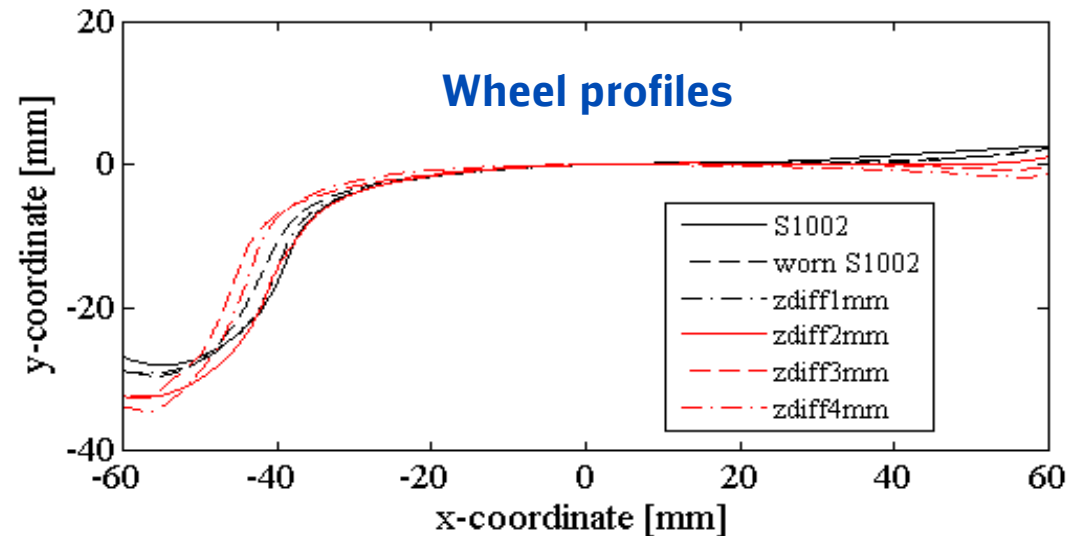




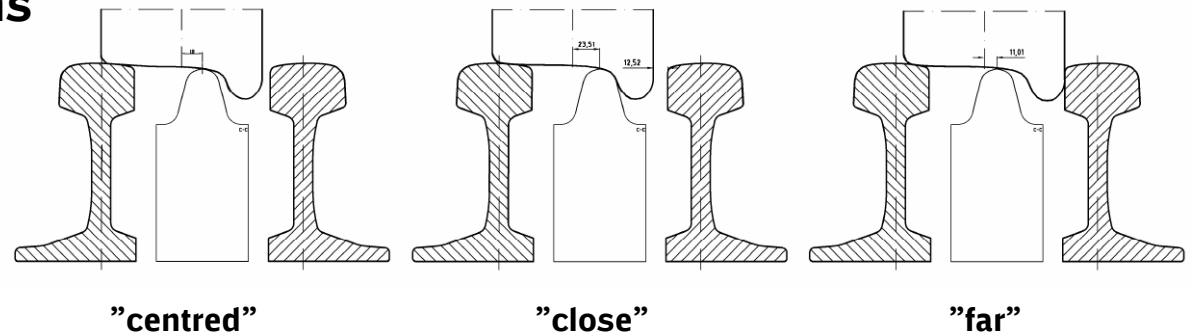
Parameter variation

Simulation Schedule

- Facing move on through route
- **Stochastic vehicle parameters:**
 - Six different wheel profiles
 - Three lateral wheel positions
 - Three vehicle speeds: 90, 120, 160 km/h
 - Two vehicle types: BR101 and BR411
- **$6 \cdot 3 \cdot 3 \cdot 2 = 108$ possible combinations**
- **Creation of a sample set based on estimated probability distributions**
- **Reduction of sample size by Latin Hypercube Sampling**



Initial lateral wheel positions on crossing entry





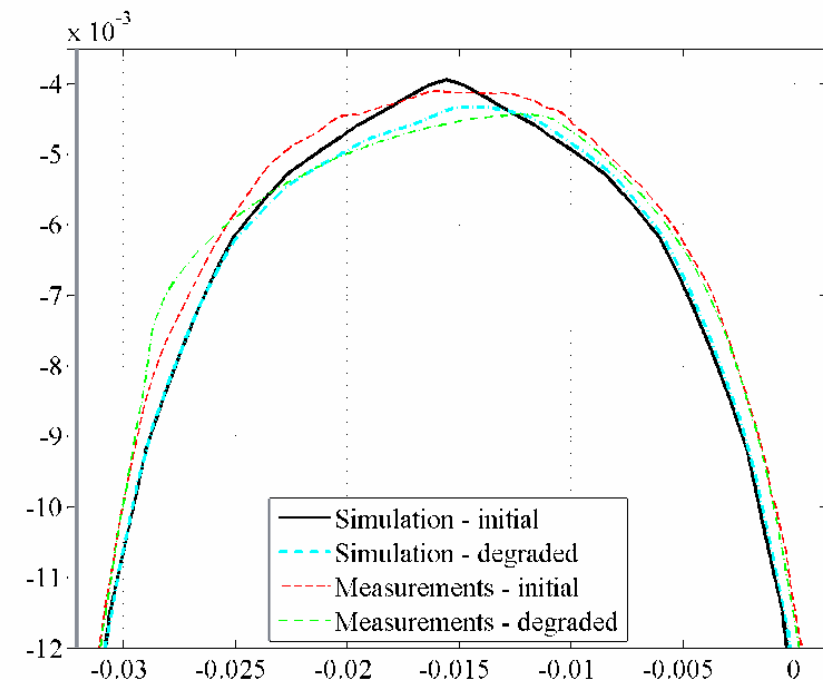
CHALMERS
CHARMEC



Simulation results

Comparison with field measurements

- **Degradation rate is larger during the first weeks after installation and then it seems to stabilise**
- **Comparison of measured and simulated profiles after five weeks of traffic**
- **Good qualitative agreement**
 - Largest degradations found for similar longitudinal positions along crossing nose
 - Same order of degradation magnitude





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Conclusions

Conclusions

- **Optimization of crossing geometry is essential to reduce the dynamic loads and consequently the Life Cycle Cost of railway turnouts.**
- **The simulation model developed by DB has been successfully validated by wayside force measurements on an in-service crossing of type EH 60-500-1:12.**
- **When comparing different crossing designs the maximum equivalent stresses calculated with CONTACT may show different trends than the maximum normal forces as the locations of the maximum stresses may differ significantly from those of the maximum forces.**
- **For relevant conclusions regarding material degradation the elasto-plastic material behavior has to be taken into account using calibrated non-linear material models.**
- **The related simulation methodology developed in INNOTRACK has been demonstrated on a crossing of R350HT steel showing good qualitative agreement between simulation and measurement after five weeks of train traffic.**



Future work

Remaining tasks

- **Validation of simulation methodology for a longer period of operation (done for 5 weeks of traffic only)**
- **Investigation of 3 different crossing materials regarding plastic deformation and wear**
- **Further improvement of crossing geometry „MaKüDe“**
- **Comparison of long-term degradation of innovative crossing geometries**



Thank you for listening!

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- [1] A. Theiler: Numerische Untersuchung der Beanspruchung im Rad-Schiene-Kontakt, Dissertation TU Berlin, 2005
- [2] D. Nicklisch, J. C. O. Nielsen, M. Ekh, A. Johansson, B. Pålsson, J. M. Reinecke, A. Zoll: Simulation of wheel rail contact forces and subsequent material degradation in switches & crossings, Proceedings 21st International Symposium on Dynamics of Vehicles on Roads and Tracks, Stockholm, 2009